The search for “smart materials” that respond to external stimuli (pH variations, ion concentration, temperature, electric field, etc.) by changes in shape or size has recently attracted considerable attention from the material research community.1–3 In addition to the obvious attractiveness of such studies in basic science, smart materials have many potential applications of great interest, including serving as the key building block for fabrication of sensors, micro-robots, micro-pumps, and actuators.

Some years ago, de Gennes4,5 first proposed using nematic liquid crystal elastomers as “artificial muscles”. The idea was to make use of a conformational change of the polymer backbone at the nematic to isotropic phase transition6 as the motor for a macroscopic contraction. On the basis of de Gennes’s idea, several thermo- and photoresponsive nematic liquid crystal elastomers have been produced.7,8 For our part, we have developed actuators using side-on nematic liquid crystal elastomers.9–11

However, all the systems described so far are “macroscopic”, that is, their size is in the millimeter/centimeter range. For numerous applications involving surface-responsive materials, such as microfluidics, micro- or nanometer-sized actuators are desirable and present an alternative to more classical responsive materials, such as piezoceramics, that have their own limitations (small displacements, need of high voltages, and incompatibility with solvent). Making use of a soft lithography technique called replica molding,12 we have succeeded in creating micron-sized responsive pillars made of nematic liquid crystal elastomers.

The required soft poly(dimethylsiloxane) (PDMS)-made molds were prepared by standard photolithography techniques. Briefly, a layer of a negative photoresist (SU80) deposited on a silicon wafer was exposed to UV light through a photomask (under a mask aligner) and developed to obtain, in relief, the desired pattern: an array of pillars 20 μm in diameter and 100 μm in height. The liquid polymer (PDMS-Sylgard 184; Dow Corning) was then poured into this mold. After cross-linking and peeling, the elastomeric replica (consisting now of an array of holes) was used itself as a “soft mold”. We irradiated through the mold using a UV lamp (30 mW·cm⁻²; λ = 365 nm; ELC-4001 light curing unit; Electro-Lite Corporation) for 30 min to promote the photo-cross-linking of the monomer mixture. After cooling to room temperature, the PDMS mold was peeled off, leaving a thin glassy polymer film covered by a regular array of pillars, as seen by optical microscopy (Figure 3). The soft mold was then gently pressed down on the melted sample, which filled the inner structure of the mold. To keep an inert atmosphere above the sample, the whole set up was then sealed in a zip-lock bag under a nitrogen flow. The temperature was then slowly decreased (−0.5 °C/min) down to 60 °C, the temperature at which the sample is in its nematic phase.9 During the cooling process, the applied magnetic field ensured the alignment of the nematic director parallel to the long axis of the pillars.

Keeping the temperature constant at 60 °C, the sample was then irradiated through the mold using a UV lamp (30 mW·cm⁻²; λ = 365 nm; ELC-4001 light curing unit; Electro-Lite Corporation) for 30 min to promote the photopolymerization—photo-cross-linking of the monomer mixture. After cooling to room temperature, the PDMS mold was peeled off, leaving a thin glassy polymer film covered by a regular array of pillars, as seen by optical microscopy (Figure 3). The soft mold was used several times without visible degradation in the quality of the obtained arrays.

When heated under the microscope, the focused picture of the top surfaces of the pillars became out of focus when the nematic to isotropic transition temperature of the elastomer was reached (around 120 °C). Cooling down to the nematic phase restored a

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Figure 3. Top view (under an optical microscope) of the pillar pattern obtained by the imprint in the nematic liquid crystal elastomer. (Inset) Zoom on the structure (pillar diameter = 20 μm).

Figure 4. An isolated pillar heated (from left to the right, the temperatures are 100, 120, and 130 °C) exhibits a contraction along its major axis of the order of 35%. Ten heating cycles (at least) do not affect this behavior.

clear picture of the pillar tops. Each pillar seemed to behave as a small actuator.

However, at this stage, we could not exclude that the contraction was due (in full or in part) to a thin responsive elastomer layer located under the pillars.

To better characterize the contraction of the posts, on a small area of the array, the pillars were cut off with a razor blade. When heated above the nematic to isotropic transition temperature, the monodisperse cylinders, suspended in silicon oil to prevent them from sticking on the glass surface, underwent a contraction that was in the order of 30–40% (Figure 4). The cylinders went back to their original size after cooling below the isotropic to nematic transition temperature (see movie S.1 in Supporting Information).

These experiments clearly demonstrate that we have successfully prepared an array of micron-sized nematic liquid single crystal elastomeric pillars that are able to contract and expand in response to small temperature changes around a well-defined transition temperature. Moreover, the size reduction improves thermal exchanges with the external medium and the time response of the contractile polymer; placed slightly above the nematic to isotropic transition temperature, a sudden cooling (by blowing air on the sample) shows qualitatively that this response is far faster than 1 s.

By reducing the characteristic size of the patterns (involving more sophisticated microfabrication methods developed for biophysics applications(14)), we have obtained similar results with pillars of 2 μm in diameter and 7 μm in height (Figure 5). However, those very small objects are much more difficult to manipulate individually than the previous ones.

These micron-sized actuators have many potential applications including the following: (1) the fabrication of active surfaces where small geometric variations often result in drastic changes of the surface properties (roughness, wettability, adhesion, etc.); (2) the achievement of small elementary ‘‘muscles’’ that can be manipulated individually and be used in micro-pumps or micro-robots.

Work is in progress to further explore the possible applications of these new thermally stimulated micro-actuators and to apply this new procedure to the preparation of light, magnetic field, or electric field stimulated micro-actuators.

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Supporting Information Available: A movie S1 (corresponding to Figure 4) showing the contraction and extension of a thermostimulable micro-actuator. This material is available free of charge via the Internet at http://pubs.acs.org.

References

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